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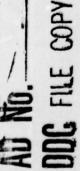
REDEFINITION AND IMPROVEMENT OF METAL VAPOR RELEASE TECHNOLOGY

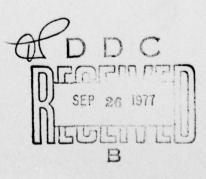
General Electric Company/RESD

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ROME AIR DEVELOPMENT CENTER Air Force Systems Command Griffiss Air Force Base, New York 13441





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REDEFINITION AND IMPROVEMENT OF METAL VAPOR RELEASE TECHNOLOGY Dr. Peter D. Zavitsanos Dr. Fred N./Alyea Mr. Joseph A./Golden tric Company/RESD Contract Number: r .-76-C-0131 Effective Date of Congract: 31 March 1976 Contract Expiration Date: 30 June 1977 Short Title of Work: Redefinition & Improvement of Metal Vapor Release Technology Subtask Number: L25BAXHX632 Period of Work Covered: Sep 76 - Jun 77 Dr. Peter D. Zavitsanos Principal Investigator: 215 962-3496 Phone: Project Engineer: Joseph J. Simons 315 330-3575 Phone: Approved for public release; RADO TR-77-269 This research was sponsored by the Defense Nuclear Agency and was monitored by Joseph J. Simons RADC (OCSA), Griffiss AFB NY 13441 under Contract/F30602-76-C-0131



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19. KEY WORDS (Continue on reverse side if necessary and identify by block number)
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ABSTRACT (Continue on reverse side if necessary and identify by block number)

This report presents the results of laboratory investigations which involved optimization studies of advanced concepts in atmospheric release technology in terms of barium vapor yield (efficiency) and increased safety. One of the most promising reactions which was identified was the reaction between Titanium and boron (in the condensed phase) to form Titanium diboride, and heat. The heat from this reaction is used to vaporize barium.

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Laboratory tests of the Titanium/Boron/Barium system produced a maximum yield of Barium vapor in the amount of 41.2% of the total mixture chemical weight.

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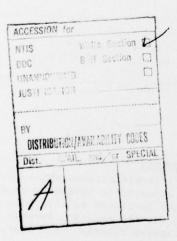


TABLE OF CONTENTS

		Page
I.	INTRODUCTION	1
II.	THERMOCHEMICAL CONSIDERATIONS	1
	A. Prediction of Barium Vapor Yield Based on the Ti/B Reaction	1
	B. Comparison of the Heat Production with Other Mixtures Used for Ion Cloud Generation	6
	C. Laboratory Results and Discussions	7
III.	ANALYSIS	11
IV.	REFERENCES	12

I. INTRODUCTION

Atmospheric experiments involving the release of metal atoms have been a subject of interest for a number of years. The release of barium vapor and its subsequent photo-ionization has been used to provide partial simulation of nuclear detonations. Barium payloads can be utilized in Transionospheric Satellite Communication programs for the purpose of performing propagation experiments in an environment which simulates certain aspects of nuclear detonation.

The objective of this effort was to (a) pursue analytical studies, computations, and consultation for the Defense Nuclear Agency's (DNA) Ad Hoc Panel for Redefinition of Barium Metal Vapor Release Technology for Advanced Communications System Program, and (b) pursue laboratory investigations which involve optimization studies of advanced concepts in atmospheric release technology in terms of barium vapor yield (efficiency) and increased safety.

II. THERMOCHEMICAL CONSIDERATIONS

A. Prediction of Barium Vapor Yield Based on the Ti/B Reaction

The high exothermicity associated with some condensed phase intermetallic reactions was identified (1, 2) as a convenient and potentially effective means of generating metal vapors for atmospheric releases. The reaction between titanium and boron has been used as heat source for atmospheric releases involving aluminum (2) as well as barium (3).

In order for a given scheme to be of practical interest, the following criteria must be satisfied: 1) Reaction can be easily initiated; 2) once initiated the reaction must be self-sustained at a fast rate; 3) the realized temperatures must be high enough to vaporize the metal of interest; 4) the system must be scalable to large quantities, and 5) the reaction should not be explosive.

As previously stated, one of the most promising reactions which was identified was the reaction between titanium and boron (in the condensed phase) to form titanium diboride according to the following stoichiometry:

$$Ti(s) + 2B(s) \longrightarrow Ti B_2(c) + heat.$$

Due to favorable thermochemical properties, this is a "gasless" reaction, i.e., the only product in addition to heat is the condensed phase of Ti $\rm B_2$; the calculated adiabatic temperature resulting from the above reaction is $4043^{\rm O}{\rm K}$.

In view of the fact that the boiling point of barium (2100°K) is considerably less than the calculated adiabatic temperature, it is safe to assume that the system can be used as "barium vaporizer" by simply adding barium to the mixture. The vapor pressure of barium in comparison to the other two components of the system (Ti and B) is shown in Figure 1. Since the vapor pressure of barium is five to six, orders of magnitude higher than that of Ti and B respectively, it is expected that extremely small amounts of gaseous titanium and boron would be generated during the barium release. Using the thermochemical properties (Table I) which govern the yield of barium vapor, the Ti/B/Ba system was balanced near the boiling point of barium:

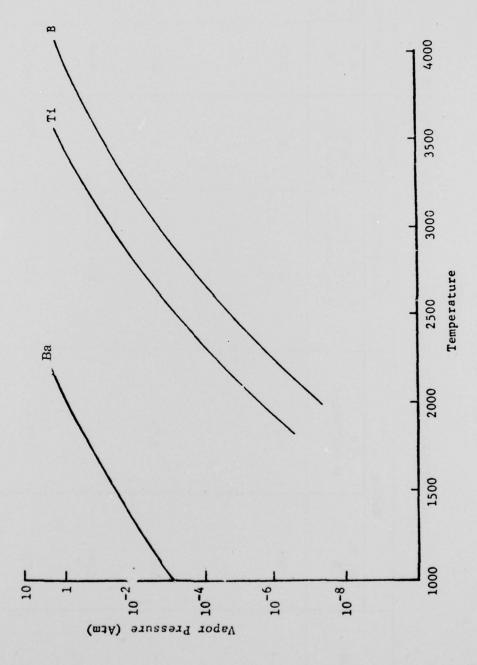


FIGURE 1. VAPORIZATION PROPERTIES

TABLEI

THERMOCHEMICAL PROPERTIES OF METALS AND COMPOUNDS (4-8)

Enthalpy Change Formation Vaporization	H_{298} $\Delta H_{f(298)}$ B. P. $\Delta H_{(298)}$ nole) (k cal/mole) (k cal/mole)	0 2100 43.9		0 3575 112.7	0 3950 129.2-137.9	-71.6
	Δ H H ₂₁₀₀ - H ₂₉₈ cal/mole) (k cal/mole)	2.3 14.0		4.0 18.3	5.1 10.1	12 ± 3
Melting	M. P. \triangle H	1000		1940	2300	3193
	Material	器	4	F		Ti B ₂

TABLE II THERMOCHEMICAL COMPARISONS

REACTION	Ba +	CuO	= BaO	+ Cu	Σ	
mol. weight	137.36	79.57	153.26	63.57	216.93	
△ H 298 (k cal/mol) - 2100	0	-37.3	-132.3	0	-95.0	
CpdT + H _{tr}			23.2	15.0	38.2	
NET AVAILABLE HEA	AT:					- 56.5 kcal/mol - 0.26 kcal/g
REACTION	2B +	Ti	= TiB ₂			
mol. weight	2x10.82	47.90	69.59		69.59	
△ Н (298)	0	0	-71.6		- 71.6	
2100						
Cp dT+H _{tr}			31.7		31.7	

NET AVAILABLE HEAT:

^{- 39.9} kcal/mol - 0.57 kcal/g

$$Ti(s) = 2 B(s) + (0.66 Ba(s)) = Ti B_2(c) + 0.66 Ba(g)$$

$$(298 OK) \qquad (2100 OK)$$

This suggests that as much as 0.66 gram-atoms (or 90.6g) of Ba could be vaporized by 1 - mole (69.59 g) of Ti B₂ which corresponds to a theoretical efficiency of 56% based on the total chemical weight.

B. Comparison of the Heat Production with Other Mixtures Used for Ion Cloud Generation

As a baseline comparison, the Ti/B/Ba system was compared with the most widely utilized reaction between Ba and CuO which forms NaO, Cu and Ba(g). The thermochemical properties of these two systems are shown in Table II.

The net available heat for barium vaporization was estimated for both cases as the difference between the exothermicity of the respective reaction minus the energy required to elevate the products to a temperature equal to the boiling point of barium $(2100^{\circ} \mathrm{K})$.

$$\triangle$$
 H available = \triangle H₍₂₉₈₎ - \bigcirc CpdT + H_{tr}

where \mathbf{H}_{tr} represents the heat of transition.

For the comparison, the amount of heat which one gram of the initial mixtures evolves is crucial; as shown in Table II, the Ba/CuO reaction evolves $\frac{56.5}{216.9}$ 0.26kcal/g while the Ti/B reaction generates $\frac{39.9}{69.54}$ 0.57 kcal/g. Therefore, the Ti/B mixture is about 2.2 times more efficient than the Ba/CuO mixture.

C. Laboratory Results and Discussion

The Ti/B/Ba mixtures were prepared in a dry box under flowing nitrogen.

The barium was in granules ranging in size from 0.1mm - 2mm and was supplied by Ventron (Beverly, Mass.). The mixtures were subsequently loaded into a graphite crucible and fired either in a vacuum tank or into a quartz tube in flowing nitrogen at one atmosphere.*

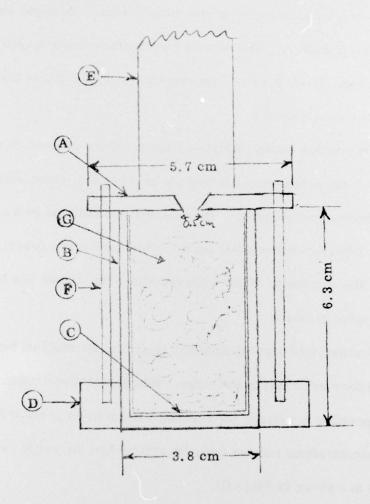
The reaction crucible shown in Figure 2 has a volume of about 70 cm³ and an orifice 0.5 cm in diameter. It is made of zirconia lined with grafoil to minimize heat losses by conduction. The reaction was initiated with a hot wire (800°C) and the vaporized barium was partly contained inside a quartz tube. Figure 3 shows the conclusion of one such run where the barium has been converted to BaO by atmospheric oxygen.

The vaporization yield was estimated by removing the residual barium from the reaction mixture by boiling in hot water. Subsequent vaporization of the water made it possible to reclaim the residual barium in the form of BaO.

Several concentrations ranging from 22-47% barium (by weight) were studied and the results are shown in Table III.

As expected from theoretical predictions, almost total removal of the available barium took place. The highest yield of 41.2% is indeed impressive. This preliminary study suggests that much higher yields, than previously possible, can now be achieved by this reaction with the additional advantage of increased safety.

^{*}A special pretreatment of the barium granules reduced drastically the oxidation rate and made it possible to carry out the firings in flowing nitrogen at one atmosphere.



A = Graphite Lid

 $B = ZrO_2$ crucible

C = Grafoil Liner

D = Base

E = Quartz Tube 1" Diameter

F = 6-32 Threaded Rod

G = Reaction Mixture



Reaction Crucible

Barium Oxide Deposit

FIGURE 3. PHOTOGRAPH OF REACTION CRUCIBLE AND OXIDIZED BARIUM DEPOSIT

TABLE III

BARIUM VAPORIZATION EFFICIENCY

orized ture Chemical Wt.)					
% Ba Vaporized (Based on Total Mixture Chemical Wt.)	19.2	21.9	26.3	29.6	41.2
Ba - Vaporized (in g)	4, 22	4.82	6.28	7.54	13.2
Ba - Recovered from Residue (g)	0.78	0.18	9.62	96.0	1.8
(in Mixture by Wt.)	22	22	28.9	33.3	46.9
Mixture	Ti/B - 17 g Ba - 5 g	Ti/B - 17 g Ba - 5 g	Ti/B - 17 g Ba - 6.9 g	Ti/B - 17 g Ba - 8.5 g	Ti/B - 17 g Ba - 15 g

The safety aspect is based on the fact that the Ti/B reaction requires a sustained high local temperature of 800°C for initiation and is insensitive to shock or electrostatic charges.

III. ANALYSIS

Consultation to the DNA/RAAE Ad Hoc Panel No. 3, "Redefinition of Barium Metal Vapor Release Technology for Advanced Communications Systems", was provided by Dr. F. N. Alyea under support of the present contract. Specifically, this effort required consultation with Dr. E. Bauer of the Institute for Defense Analysis and emphasized preparation of the Panel report entitled, "Barium Releases for Communications Experiments."

The work involved writing Chapter V, "Barium Release Phenomenology", general report organization, and considerable text editing, particularly in the appendicies. The report has been submitted to DNA for approval.

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